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Mantle dynamics inferred from the crystallographic-preferred-orientation of bridgmanite

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Keywords: bridgmanite, shear deformation, slip system, seismic anisotropy, lower mantle

Bridgmanite, (perovskite-structured (Mg,Fe)SiO₃) is the dominant constituent mineral in the Earth's lower mantle but its rheological properties are largely unknown. Seismic shear wave anisotropies¹⁻⁶ are observed in the Earth's uppermost lower mantle around several subducted slabs. The anisotropy caused by deformation-induced crystallographic-preferred-orientation (CPO) of bridgmanite is the most plausible candidates of this feature. Uniaxial deformation experiments⁷⁻⁹ have been carried out to determine the deformation texture of bridgmanite but the dominant slip system (slip direction and plane) has not been determined. Here we report the CPO pattern and dominant slip system of bridgmanite under uppermost lower mantle conditions (25 GPa and 1873 K) obtained for the first time through simple shear deformation experiments using the Kawai-type deformation-DIA apparatus¹⁰. The obtained fabrics are characterized by the a-axis perpendicular to the shear plane and the c-axis parallel to the shear direction, implying that the dominant slip system of bridgmanite is [001](100). The observed shear wave anisotropies near subducted slabs¹⁻⁴ (Tonga-Kermadec, Kurile, Peru and Java) are explained by the CPO of bridgmanite induced by flow directions along the strike on the plates. Flow direction in the lower mantle would be determined based on a combination of the CPO of bridgmanite and seismic observations¹⁻⁶.

Recent P-wave seismic tomography¹¹ revealed four types of geometry of subducted slabs in the mantle: I - slab stagnant above the 660 km discontinuity; II - slab penetrating the 660 km discontinuity (e.g. Kuril); III - slab lying in the uppermost lower mantle between a depth of 660–1000 km (e.g. Tonga-Kermadec, Sumatra and South America); and IV - slab continuously descending into the mid lower mantle. Seismic tomography¹¹⁻¹³ provides morphological images of the subducted slabs in the Earth's mantle, but does not give any insight into the dynamic features of the slab. However, seismic anisotropy observed in the mantle provides information on the flow direction of the slabs in the deep mantle because the anisotropy may be the reflection of the crystallographic-preferred-orientation (CPO) of the constituent minerals yielded by dislocation creep deformation.

As shown in previous reports, a significant anisotropy demonstrating clear shear wave splitting was observed in the uppermost lower mantle of the Tonga-Kermadec slab region^{1,2}. Recently, such anisotropies were also observed in the uppermost lower mantle of slab regions³⁻⁵. In these observations, shear wave splitting shows fast polarization generally parallel to the plane of the subducted plate (e.g. Tonga-Kermadec, Java, Peru and Kurile)¹⁻⁴ while other observed slab regions do not show a consistent

splitting pattern³. Therefore, it is interesting to examine how the observed shear-wave anisotropy could be interpreted by the CPO of the lower mantle minerals. It is generally accepted that in pyrolitic mantle model, the constituents of the lower mantle are bridgmanite (77 vol. %), (Mg,Fe)SiO₃-perovskite of space group *Pbnm*, ferropericlasite (16 vol. %), and CaSiO₃-perovskite (7 vol. %)¹⁴. The contribution of the CPO of ferropericlasite is negligible because of its nearly isotropic elasticity at the uppermost lower mantle conditions¹⁵. CaSiO₃-perovskite is elastically anisotropic¹⁶ but the contribution of this phase to seismic anisotropy will not be significant because of the small amount of CaSiO₃ in the lower mantle. In contrast, it is anticipated that the significant seismic anisotropy can be produced by the CPO of bridgmanite^{17,18}, based on its high elastic anisotropy^{19,20} and overwhelming presence in the lower mantle. Thus, we focused on the deformation-induced CPO of bridgmanite as the most important factor of the plausible lower mantle seismic anisotropy.

We performed shear deformation experiments of bridgmanite with controlled strain rate under lower mantle conditions employing the deformation-DIA (D-DIA) type multi-anvil press with the Kawai-type cell assembly (6-8 type)¹⁰. Dense sintered (Mg_{0.97}Fe_{0.03})SiO₃ bridgmanite aggregates synthesized at 25 GPa and 1873 K were used as samples for the deformation experiments. A backscattered electron image (Figure

1(a)) and pole figures (Figure 2(a)) of sintered bridgmanite revealed that the sample was an equigranular aggregate with a typical grain size of 15 μm and a random crystallographic orientation, which was determined by 2D monochromatic X-ray diffraction pattern method (see Methods). In the deformation experiments, a thin ellipse of bridgmanite aggregate with a strain marker of Ni foil, which was initially set at the middle of the sample perpendicular to the cut surfaces of the alumina pistons, was sandwiched between 45°-cut polycrystalline dense alumina pistons at the centre of the cell assembly. Corresponding to the advancement of the differential rams of the D-DIA press, the alumina pistons apply simple shear to the thin bridgmanite sample.

Figures 1(b) and (c) show the microstructures of the recovered samples from the undeformed (only annealing) experiment (run K116) and from the deformation experiment (run K122), respectively, both performed at identical P/T conditions (25 GPa, 1873 K). In the former, the strain marker was almost normal to the cut surfaces of the alumina pistons, showing that the shear strain of the bridgmanite sample was very close to zero. Thus the sample was almost free from deformation through all the processes; i.e., compression, heating, annealing, and subsequent decompression. As shown in Figure 1(c), the strain marker definitely tilted in the deformed sample. From the tilting angle of the strain marker ($\sim 38^\circ$) and the deformation time (1 h), the total

strain and average strain rate were determined to be $\gamma \sim 0.8$ and $\dot{\gamma} \sim 2 \times 10^{-4}$ /s, respectively. Thickness of the deformed sample was reduced by about 20% in comparison with the original, suggesting the presence of some amount of uniaxial component of the deformation. The microstructural observation in Figure 1(d) shows that the elongated bridgmanite grains of sizes up to 30-40 μm declined along the shear direction and are surrounded by small grains of less than a few micrometres. The structural features indicate that dynamic recrystallization occurred, and hence, CPO of bridgmanite could be induced by deformation involving dislocations.

The crystallographic orientation of the bridgmanite was determined using the 2D monochromatic X-ray diffraction pattern method^{7,9,21} for both the starting and deformed samples. The sheared bridgmanite aggregate demonstrated strong fabric (Figure 2b), whereas the starting material did not show significant CPO pattern (Figure 2a). In the sheared bridgmanite, the [100] axis was oriented perpendicular to the shear plane. Although weak girdle patterns of the [001] and [010] axes corresponding to uniaxial compressive strain were observed, the [001] and [010] axes were mostly aligned parallel and normal to the shear direction on the shear plane, respectively. Experimental textures are compatible with an orientation-producing deformation mechanisms such as dominant slip on [001](100) under conditions of 25 GPa and 1873 K, corresponding to

the uppermost lower mantle conditions.

The dominant slip system of bridgmanite at a high deviatoric stress condition was reported through high pressure experiments^{7,8,22} and theoretical calculations^{18,23}, as shown in Extended data Table 1. Using a diamond anvil cell, uniaxial deformation experiments of bridgmanite were conducted at room temperature^{7,22}. No clear CPO pattern was observed⁷, probably due to insufficient strain while dominant slip systems were reported as [100], [010] and <110> on (001) below 55 GPa and (100) plane over 55 GPa²². Uniaxial stress relaxation experiments (USRE) of bridgmanite were carried out using the Kawai-type multianvil press at 25 GPa and 1673 K⁸. Analysis of the recovered samples using the X-ray peak broadening technique suggested that the dominant slip direction is the [100] in contradiction to the present results. Dense deformation bands across the pre-existing twin boundaries observed in the USRE⁸ suggested that the bridgmanite aggregate was deformed under very high deviatoric stress. Such an extremely high deviatoric stress, up to several GPa by compression at room temperature, was directly measured during in-situ USRE of olivine polymorphs^{24,25}. The [100] slip direction observed by USRE of bridgmanite⁸ might be the result under very high deviatoric stress condition.

The [100](001) slip system was reported to be one of the most easily activated

slip systems of bridgmanite in the dislocation glide region by a first principles calculation²³, supporting that the observed slip direction by USRE results from dislocation glide, whereas other study by first principles calculations with visco-plastic self-consistent model¹⁸ suggested that the most easily activated slip system is [010](100) at 0 K and a pressure range between 0 to 100 GPa in the dislocation glide region. Both calculations and previous experimental results are inconsistent with the present results. This could be due to the differences of dominant slip mechanisms or dominant deformation mechanisms by variation of experimental conditions (e.g. stress, temperature and pressure) such as in the case of olivine²⁶.

CaTiO₃-perovskite is often used as an analogue material for bridgmanite because of their similar rotation angles of the SiO₆ or TiO₆ octahedron. Uniaxial deformation experiments were performed on CaTiO₃-perovskite²⁷, in which dislocation creep is expected due to high temperature (up to 1973 K) and low deviatoric stress (25-120 MPa). TEM observations of the recovered sample revealed that screw dislocation with Burgers vectors [100]_{pc} and [011]_{pc} on the (01-1)_{pc} plane, where indexing is based on the pseudo-cubic (pc) system, formed rectangular networks. The [100]_{pc} and [011]_{pc} directions on the (01-1)_{pc} plane in pseudo-cubic indexation of perovskite include the 1/2[001] and [010] directions on the (100) plane in the orthorhombic system. The

[001](100) slip system in the present study does not contradict with that of CaTiO₃-perovskite.

The seismic wave anisotropy formed by the CPO of deformed bridgmanite in the present study was calculated based on the elastic constant¹⁹ as shown in Figure 3. For the shear wave anisotropy of deformed bridgmanite, the velocity of horizontally polarized shear waves, V_{SH} , is $\sim 1\%$ higher than that of vertically polarized shear waves, V_{SV} , in horizontal flow as shown in Figure 3(b), whereas V_{SV} is 0.03-1.10% higher in vertical flow in Figure 3(d). As shown in Figure 4(a), shear wave splitting with $V_{SH} > V_{SV}$ are observed in the uppermost lower mantle from the Tonga-Kermadec subduction zone to the Australian continental seismic stations, where the ray path is nearly parallel to the section^{1,2}. The delay time ranges from 0.7 to 6.2 s^{1,2}, which corresponds to average $(V_{SH} - V_{SV})/V_{SV} \sim 0.1-1\%$ assuming a 3000–6000 km ray path including 1000-2000 km subducted plate region¹¹ on the uppermost lower mantle. The magnitude of the shear wave anisotropy is consistent with deformed bridgmanite in the present study as shown in Figure 3(b). In contrast, opposite shear wave anisotropy ($V_{SV} > V_{SH}$) was observed from the Tonga-Kermadec subduction zone to the western North America stations, where the ray path is nearly perpendicular to the section⁴. It is thus concluded, that both of the observed shear-wave anisotropies around the Tonga-Kermadec subduction zone,

which are type III in the P-wave tomography¹¹, are well explained by the CPO of bridgmanite yielded by the penetration of subducted slabs down to 1000 km by vertical motion and by the stagnation at around 1000 km depth with a horizontal flow in the pyrolitic mantle as shown in Figure 4(a). This flow pattern could be caused by the viscosity hill²⁸⁻³⁰ at depths between 1000 and 1500 km, and the viscosity reduction of the slab by interconnection of ferropericlase in the post-spinel phase³¹. Shear wave anisotropies at the top of the lower mantle beneath Java (type III), Peru (type III), and Kuril subducted slabs (type II) were observed along the seismic ray path nearly parallel to the subducted plate surface³ (Figure 4 b-d). In these observations, the fast polarization in shear wave splitting appear to be arranged generally parallel to the plane of the plate³, which is explained by the deformation-induced CPO of bridgmanite formed by the parallel flow to the subducting direction. Therefore, the present results on CPO of bridgmanite coupled with the observation of seismic anisotropy provides a strong evidence to understand the direction of the mantle flow, which can be often expected from seismic tomography.

Figure captions

Figure 1. Backscattered electron images of the bridgmanite aggregates. (a): sample sintered, (b): sample annealed at 25 GPa and 1873 K for 10 min (run K116), (c) and (d): sample deformed at 25 GPa and 1873 K for 1 h (run K122). In (a) and (d), polished surfaces were etched with colloidal silica to clarify grain boundaries. In (b) and (c), black arrows indicate Ni foil strain markers. The strain marker in the annealed sample in (b) remains perpendicular to the 45°-cut surfaces of alumina pistons, indicating almost no deformation during compression and annealing. In (c), tilting of the Ni strain marker to 38 ° in the deformed sample indicating a strain of $\gamma \sim 0.8$. Elongated grains, indicating dynamic recrystallization, were only observed in the deformed sample indicated by the gray arrow in (d). X, Y, and Z coordinates correspond to the shear direction, shear plane normal, and perpendicular to both “X” and “Y” directions, respectively. This definition of coordinates is used in Figures 2 and 3 and in extended data Figure 7.

Figure 2. Pole figures of bridgmanite showing the variation of crystallographic orientation of the [100], [010] and [001] directions in the coordinate system defined with respect to the deformation geometry of bridgmanite (a) sintered and (b) deformed

(K122) at $\gamma \sim 0.8$ and $\dot{\gamma} \sim 2 \times 10^{-4}$ /s. Black dashed lines represent the long axis of the ellipsoid strain of the deformed bridgmanite.

Figure 3. Seismic wave anisotropy of bridgmanite aggregates deformed in shear under the uppermost lower mantle pressures and temperatures (25 GPa and 1873 K) (run K122) calculated using a software³². (a) and (c) P-wave seismic velocity at horizontal and vertical flow, respectively. (b) and (d) Trace of the V_{S1} polarization plane at horizontal and vertical flow, respectively.

Figure 4. Schematic cross-sections of subducted slabs of (a) the Tonga-Kermadec arc (b) Java arc, (c) Peru arc, and (d) Kuril arc based on P-wave tomography¹¹. Blue and orange lines represent shear seismic ray paths nearly parallel and perpendicular to the section for the observation of shear wave anisotropies at the Tonga-Kermadec slab^{1-2,4} and Kuril, Peru and Java slabs³, respectively. Blue and orange polar histograms show polarization of the fast shear wave perpendicular to blue and orange seismic ray paths of the Tonga-Kermadec slab^{1,2,4} Kuril, Peru and Java slabs³, respectively. The fast polarization arrangement is almost parallel to the plane of the subducted plates. Yellow dashed lines correspond to flow directions of the subducted slab. Black double arrows

represent shear directions. The uppermost lower mantle near the subducted slab is deformed by the flow directions parallel to the subducted slab, which align the a - and c -axis of bridgmanite from normal to shear deformation plane and parallel to shear direction, respectively.

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Acknowledgement

We appreciate to help by E. Ito to prepare manuscript, Takahashi Lab and HACTO group member to collect 2D diffraction and T. Ohuchi, and D. Mainprice's codes to calculate seismic anisotropy of bridgmanite. Official review by two anonymous reviewers improved the quality of the manuscript. This work was supported by JSPS KAKENHI Grant Number 15J09669 to NT. The 2D diffraction measurements for analysis of LPO were carried out on the BL04B1 at SPring-8 under the approval with JASRI (Proposal Nos. 2012B1437, 2013B1434, 2014A1431, 2014B1400, 2015A1600 and 2015B1504).

Author Contributions: NT planned the present study. NT performed deformation experiments with help for YN, DY, and ET. NT and DY collected 2D diffraction pattern with help for YH. NT analyzed crystal orientation distribution of bridgmanite aggregate with help for YS. NT, DY, and YN wrote the manuscript.

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